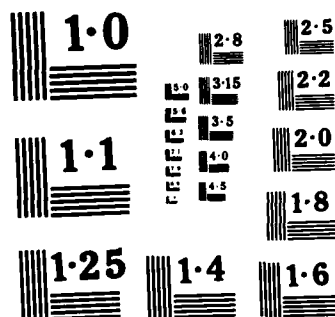


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CONTROL FOR THE STABILIZATION OF ANY STRICTLY
PROPER MINIMUM PHASE LINEAR SYSTEMS WITH RELATIVE
DEGREE NOT EXCEEDING TWO AND DIMENSION NOT EXCEEDING n

A. S. Morse
Department of Electrical Engineering¹
Yale University
New Haven, Connecticut
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INTRODUCTION

In a recent paper [1] it was shown that there are smooth, nonlinear, three-dimensional controllers, not incorporating probing signals, which are capable of adaptively stabilizing any single-input, single-output, minimum phase, relative degree two or less linear system of any dimension. Controllers of this type are based on minimal dynamic compensator synthesis [2]. While such controllers are simple in structure they do not have a model-following capability.

In this paper we develop a new algorithm based on observer theory [2], which can adaptively stabilize and achieve model-following as well. The controller, which is a smooth nonlinear dynamical system of dimension $4(n+1)$, can adaptively stabilize any physical process with scalar input u and scalar output y , provided the process can be modelled by a strictly-proper, minimum phase, linear system of dimension not exceeding n and relative degree not exceeding two. The controller is based on concepts developed previously in [1] and [3].

1. CONTROL EQUATIONS

The controller to be examined consists of a two-dimensional reference system

$$\begin{aligned}\dot{y}_r + \lambda_1 y_r &= \rho \\ \dot{\rho} + \lambda_2 \rho &= r\end{aligned}\tag{1}$$

where λ_1 and λ_2 are positive constants and $r(\cdot)$ is a bounded, differentiable reference input, a tracking error

$$e = y - y_r,\tag{2}$$

sensitivity function n-vectors θ_u and θ_y generated by the equations

$$\begin{aligned}\dot{\theta}_u &= A\theta_u + bu \\ \dot{\theta}_y &= A\theta_y + by\end{aligned}\tag{3}$$

where n is a prespecified positive integer and (A,b) is any n -dimensional controllable pair with A stable, and a control law

$$u = N(\|k\|)(k'_u \theta_u + k'_y \theta_y + k'_\rho \rho + k'_r r)\tag{4}$$

where k_u, k_y, k_ρ and k_r are control parameters,

$$k = [k'_u, k'_y, k'_\rho, k'_r]^T,\tag{5}$$

$\|k\| = (k'k)^{1/2}$, and $N(\cdot)$ is a Nussbaum Gain, i.e. any integrable function satisfying

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$$\begin{aligned} \sup_{\xi > 0} \left\{ \frac{1}{\xi} \int_0^{\xi} \mu N(\mu) d\mu \right\} &= \infty \\ \inf_{\xi > 0} \left\{ \frac{1}{\xi} \int_0^{\xi} \mu N(\mu) d\mu \right\} &= -\infty \end{aligned} \quad (6)$$

(e.g., $N(\mu) = \mu^2 \cos(\mu^2)$). Control parameters k_u, k_y, k_ρ and k_r are adjusted according to the rules

$$\begin{aligned} k_u &= \theta_u e + z_u & \dot{z}_u &= \lambda_1 \theta_u e - (A\theta_u + bu)e \\ k_y &= \theta_y e + z_y & \dot{z}_y &= \lambda_1 \theta_y e - (A\theta_y + by)e \\ k_\rho &= \rho e + z_\rho & \dot{z}_\rho &= \lambda_1 \rho e - (r - \lambda_2 \rho)e \\ k_r &= re + z_r & \dot{z}_r &= \lambda_1 re - \dot{r}e \end{aligned} \quad (7)$$

The controller defined by (1)-(7) may be viewed as a smooth $4(n+1)$ -dimensional dynamical system with inputs r, \dot{r} and y , state $\{y_r, \rho, \theta_u, \theta_y, z_u, z_y, z_\rho, z_r\}$ and output u .

Remarks:

1. By using minimal dimensional observer theory, it is possible to reduce the dimensions of θ_u and θ_y to $(n-1)$ and to eliminate one control parameter thereby obtaining a $(4n+1)$ -dimensional algorithm with the same capabilities as the one described here [2]. The stability analysis of the lower-dimensional algorithm is essentially the same as the analysis which follows.
2. There are two different ways to avoid generating the derivative of the reference signal r required by the above algorithm. The first is simply to introduce a new reference signal \bar{r} and then make r a state of a three-dimensional reference system defined by (1) and $\dot{\bar{r}} + \lambda_3 r = \bar{r}$ where $\lambda_3 > 0$. The second is to make use of an idea due to Monopoli [4,5] which amounts to replacing (4) and (7) by

$$u = N(\|k\|)k'\theta + \left(\frac{(k'\phi)^2}{2\|k\|} \right) \frac{\partial N(\|k\|)}{\partial \|k\|} + N(\|k\|)\phi'\phi)e$$

and

$$\dot{k} = \phi e$$

respectively where

$$\theta = [\theta_u', \theta_y', \rho, r] \quad (8)$$

and $\dot{\phi} + \lambda_2 \phi = \theta$. This alternative, however, requires $N(\cdot)$ to be differentiable.

2. MAIN RESULT

The process to which the preceding algorithm is applicable must admit a minimum phase, linear model of dimension $n \leq n$ and relative degree ≤ 2 . It is known [6] that these assumptions imply that such a process can also be modelled by a n -dimensional, stabilizable, minimum phase, relative degree two or one linear system of the form

$$\begin{aligned} \dot{x}_p &= (A + h_p c)x_p + b_p u \\ y &= cx_p \end{aligned} \quad (9)$$



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where c is any row vector chosen so that (c, A) is observable, and k_p and b_p are unknown constant, parameter vectors. We take (9) as the model of the process to be controlled. Our main result is as follows.

Theorem 1: For each initial state and each differentiable input r , bounded on $[0, \infty)$, the state response $X = \{x_p, \theta_u, \theta_y, \rho, y_r, z_u, z_y, z_\rho, z_r\}$ of the closed-loop system defined by (1)-(9) exists and is bounded on $[0, \infty)$ and the tracking error $e \rightarrow 0$ as $t \rightarrow \infty$.

The remainder of this paper is devoted to a proof of this theorem.

3. STABILITY ANALYSIS

To prove Theorem 1, it proves useful to work with a certain system of equations which we now derive. For this let n^* denote the relative degree of (9) and define

$$\delta = \dot{y} + \lambda_1 y \quad (10)$$

It is known [6] that for $n^* = 1$,

$$\delta = gu - d_u' \theta_u - d_y' \theta_y + \epsilon \quad (11)$$

where g is a nonzero constant - the "high-frequency gain" - d_u and d_y are unknown parameter vectors, and ϵ is an unknown linear combination of decaying exponentials. Similarly, for $n^* = 2$ it is known that

$$\dot{\delta} + \lambda_2 \delta = gu - d_u' \theta_u - d_y' \theta_y + \epsilon \quad (12)$$

where g , d_u , d_y and ϵ have the same interpretations as for $n^* = 1$. It is also known [6] in either case that if $\bar{x} = [\theta_u', \theta_y', x_p']'$, then \bar{x} satisfies

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{b}(gu - d_u' \theta_u - d_y' \theta_y + \epsilon) \quad (13)$$

where \bar{A} is stable.

To proceed, define

$$\sigma = \dot{e} + \lambda_1 e \quad (14)$$

and note from (1), (2) and (10) that $\sigma = \delta - \rho$. It follows from (1), (11) and (12) that

$$\sigma = gu - d_u' \theta_u - d_y' \theta_y + \epsilon - \rho$$

if $n^* = 1$ and

$$\dot{\sigma} + \lambda_2 \sigma = gu - d_u' \theta_u - d_y' \theta_y + \epsilon - r$$

if $n^* = 2$. Thus if we define $d = [d_u', d_y', 1, 0]'$ for $n^* = 1$ or $d = [d_u', d_y', 0, 1]'$ for $n^* = 2$, then

$$\sigma = gu - d' \theta + \epsilon \quad \text{if } n^* = 1 \quad (15)$$

and

$$\dot{\sigma} + \lambda_2 \sigma = gu - d' \theta + \epsilon \quad \text{if } n^* = 2 \quad (16)$$

where θ was defined previously in (8). If in addition we define $q = [1, 0]'$ for $n^* = 1$ or $q = [0, 1]'$ for $n^* = 2$, then for $n^* = 1$ or 2 (13) becomes

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{b}(gu - d' \theta + \epsilon + [\rho, r]q) \quad (17)$$

Thus with the notation

$$\bar{u} = gu - d'\theta + \epsilon,$$

(15) through (17) can be rewritten as

$$\sigma = \bar{u} \quad \text{if } n^* = 1 \quad (15)'$$

$$\dot{\sigma} + \lambda_2 \sigma = \bar{u} \quad \text{if } n^* = 2 \quad (16)'$$

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{b}(\bar{u} + [\rho, r]'q) \quad (17)'$$

By differentiating the expressions for k_u, k_y, k_ρ and k_r in (7) and substituting in the expressions for $\dot{z}_u, \dot{z}_y, \dot{z}_\rho, \dot{z}_r$ also in (7), it is straightforward to verify that $\dot{k}_u = \theta_u \sigma$, $\dot{k}_y = \theta_y \sigma$, $\dot{k}_\rho = \rho \sigma$ and $\dot{k}_r = r \sigma$, σ being given by (14). Using (5) and (8) we can thus write

$$\dot{k} = \theta \sigma \quad (18)$$

For ease of reference we now summarize in one place, the system of equations to be analyzed.

$$\dot{e} + \lambda_1 e = \sigma \quad (19a)$$

$$\sigma = \bar{u} \quad \text{if } n^* = 1 \quad (19b)$$

$$\dot{\sigma} + \lambda_2 \sigma = \bar{u} \quad \text{if } n^* = 2 \quad (19c)$$

$$\bar{u} = gN(\|k\|)k'\theta - d'\theta + \epsilon \quad (19d)$$

$$\dot{k} = \theta \sigma \quad (19e)$$

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{b}(\bar{u} + [\rho, r]'q) \quad (19f)$$

$$\dot{\rho} + \lambda_2 \rho = r \quad (19g)$$

$$\theta = [\theta'_u, \theta'_y, \rho, r]' \quad (19h)$$

$$\bar{x} = [\theta'_u, \theta'_y, x'_p]' \quad (19i)$$

The preceeding defines a dynamical system of the form $\dot{Z} = F(Z, r, \epsilon)$ where $Z = [e, \sigma, k, \bar{x}, \rho]$ (with σ deleted from Z if $n^* = 1$). Observe that boundedness of Z implies boundedness of $e, \sigma, k, \theta_u, \theta_y, x_p$ and ρ . Boundedness of ρ together with (1) implies boundedness of y_r . In addition, boundedness of $e, k, \theta_y, \theta, \rho$ and r together with (5) and (7) imply boundedness of z_u, z_y, z_ρ and z_r . Thus to prove Theorem 1 it is enough to show that $Z(t)$ exists and is bounded on $[0, \infty)$ and that $e(t) \rightarrow 0$ as $t \rightarrow \infty$.

Differentiability of F implies that for any initial state $Z(0)$, there must exist an interval $I = [0, t_1]$ on which a solution $Z(t)$ exists. For any function $\xi(t)$ defined on I , we write $\xi \in L^\infty(I)$ if $\|\xi\| = \sqrt{\xi' \xi}$ is bounded on I by a constant not depending on t_1 ; we also write $\xi \in L^2(I)$ if $\int_0^{t_1} \|\xi(\tau)\|^2 d\tau \in L^\infty(I)$.

We can now state

Proposition 1: There exist constants C_1 and C_2 , not depending on t_1 , such that for $t \in I$

$$\int_0^t \sigma(\tau) \bar{u}(\tau) d\tau \leq g\pi(\|k(t)\|) + \frac{\lambda_2}{1+\lambda_2} \int_0^t \sigma^2(\tau) d\tau + C_1 \|k(t)\| + C_2 \quad (20)$$

where

$$\pi(\xi) = \int_0^\xi \mu N(\mu) d\mu \quad (21)$$

Proof: Set $\eta = \|k\|^2$; hence from (19e), $\dot{\eta} = 2k'\theta\sigma$. It follows from this, (19d) and (19e) that

$$\sigma \bar{u} = \frac{g}{2} N(\eta^{1/2}) \dot{\eta} - d' \dot{k} + \sigma \epsilon \quad (22)$$

We can now develop bounds for the integrals of the terms on the right side of (22).

First note that

$$\begin{aligned} g/2 \int_0^t N(\eta^{1/2}(\tau)) \dot{\eta}(\tau) d\tau &= g/2 \int_{\eta(0)}^{\eta(t)} N(\eta^{1/2}) d\eta \\ &= g \int_{\|k(0)\|}^{\|k(t)\|} \omega N(\omega) d\omega \end{aligned} \quad (23)$$

Next observe that

$$\begin{aligned} - \int_0^t d' \dot{k}(\tau) d\tau &= d' k(0) - d' k(t) \\ &\leq \|d\| \|k(t)\| + |d' k(0)| \end{aligned} \quad (24)$$

For any positive constant C , $\sigma \epsilon \leq C\sigma^2 + \epsilon^2/4C$. Thus

$$\int_0^t \sigma(\tau) \epsilon(\tau) d\tau \leq C \int_0^t \sigma^2(\tau) d\tau + \frac{1}{4C} \int_0^t \epsilon^2(\tau) d\tau \quad (25)$$

By setting $C = \lambda_2/(1+\lambda_2)$, $C_1 = \|d\|$ and

$$C_2 = |g\pi(\|k(0)\|)| + |d' k(0)| + \frac{1}{4C} \int_0^\infty \epsilon^2(\tau) d\tau,$$

(23)-(25) can be combined to yield (20). \square

Proof of Theorem 1: From (19b) and (19c) it follows that $\int_0^t \sigma(\tau) \bar{u}(\tau) d\tau$ equals $\int_0^t \sigma^2(\tau) d\tau$ if $n^* = 1$ or $\lambda_2 \int_0^t \sigma^2(\tau) d\tau + \frac{1}{2}(\sigma^2(t) - \sigma^2(0))$ if $n^* = 2$. This and Proposition 1 thus imply that

$$\Omega(\|k(t)\|) \geq \left\{ \begin{array}{ll} \frac{1}{(1+\lambda_1)} \int_0^t \sigma^2(\tau) d\tau & \text{if } n^* = 1 \\ \frac{\lambda_1^2}{(1+\lambda_1)} \int_0^t \sigma^2(\tau) d\tau + \frac{\sigma^2(t)}{2} & \text{if } n^* = 2 \end{array} \right\} \quad (26)$$

where

$$\Omega(\xi) = g\pi(\xi) + C_1 \xi + C_2 + \sigma^2(0)/2$$

In view of (6) and the definition of $\pi(\xi)$ in (21) it is easy to see that there must exist a closed-bounded interval $[a, b]$ containing $\|k(0)\|$ for which both $\Omega(a)$ and

$\Omega(b)$ are negative. Since (26) implies that for any $t \in I$, $\Omega(\|k(t)\|) \geq 0$, $\|k(t)\|$ cannot pass through either a or b. Therefore $\|k\| \in L^\infty(I)$. In addition, since $\Omega(\xi)$ is continuous, it follows from (26) that $\sigma \in L^2(I)$ for $n^* = 1$ and $\sigma \in L^2(I) \cap L^\infty(I)$ for $n^* = 2$. Thus $\sigma \in L^2(I)$ for $n^* = 1, 2$ so by (19a) $e \in L^2(I) \cap L^\infty(I)$ for $n^* = 1, 2$.

For $n^* = 1$, $\bar{u} = \sigma \in L^2(I)$; since $[\rho, r]' \in L^\infty(I)$ it follows from (19f) that $\bar{x} \in L^\infty(I)$.

For $n^* = 2$, $\bar{u} = \dot{\sigma} + \lambda_2 \sigma$ and $\sigma \in L^\infty(I)$; again it follows from (19f) that $\bar{x} \in L^\infty(I)$.

At this point we have shown that $Z = [e, \sigma, k, \bar{x}, \rho]' \in L^\infty(I)$ for $n^* = 2$, that $Z = [e, k, \bar{x}, \rho]' \in L^\infty(I)$ for $n^* = 1$ and that $e \in L^2(I)$ for $n^* = 1, 2$. Therefore we can take $t_1 = \infty$. Thus Z is bounded on $[0, \infty)$ and $e \in L^2[0, \infty)$. In addition, since (19) implies that $\dot{e} \in L^\infty(0, \infty)$, it follows that $e \rightarrow 0$ as $t \rightarrow \infty$. \forall

CONCLUDING REMARKS

The algorithm presented here and its subsequent stability analysis rely for the most part on ideas developed previously in [1], [3] and [6]. In fact the stability analysis given is almost identical to that used in [1]. The essential new idea in this paper is to use a control law (4) incorporating both reference model state ρ and reference input r . It is this departure from more traditional adaptive control laws, (e.g. [3]) which makes model following possible with one algorithm for processes of both relative degree 1 and 2.

REFERENCES

- [1] Morse, A.S., A 3-dimensional "universal" controller for the adaptive stabilization of any strictly proper, minimum phase system with relative degree not exceeding two, IEEE Trans. Auto. Control, (December 1985), to appear.
- [2] _____, New directions in parameter adaptive control, Proc. 1984 IEEE Conf. on Decision and Control, Las Vegas, pp. 1566-1568.
- [3] _____, An adaptive control for globally stabilizing linear systems with unknown high-frequency gains, Proc. Sixth International Conference on Analysis and Optimization of Systems, in: Springer Lecture Notes in Control and Information Sciences, 62, (June 1984) pp. 58-68.
- [4] Monopoli, R.V., Model reference adaptive control with an augmented error signal, IEEE Trans. Auto. Control, AC-19, (Oct. 1974) pp. 474-484.
- [5] Feuer, A. and Morse, A.S., Adaptive control of single-input, single-output linear systems, *ibid*, AC-23, (August 1978) pp. 557-569.
- [6] Morse, A.S., Global stability of parameter-adaptive control systems, *ibid*, AC-25, (June 1980) pp. 433-439.

FOOTNOTES

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